# NASA Contractor Report 158942

00/24 31565

# PROCESS IDENTIFICATION STUDY FOR SPACE CURED COMPOSITE STRUCTURES

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CONTRACT NAS1-14887-Task 1 September 1978

(NASA-CR-158942) PROCESS IDENTIFICATION STUDY FOR SPACE CURED COMPOSITE STRUCTURES (lockheed Missiles and Space Cc.) 19 p

N89-70002

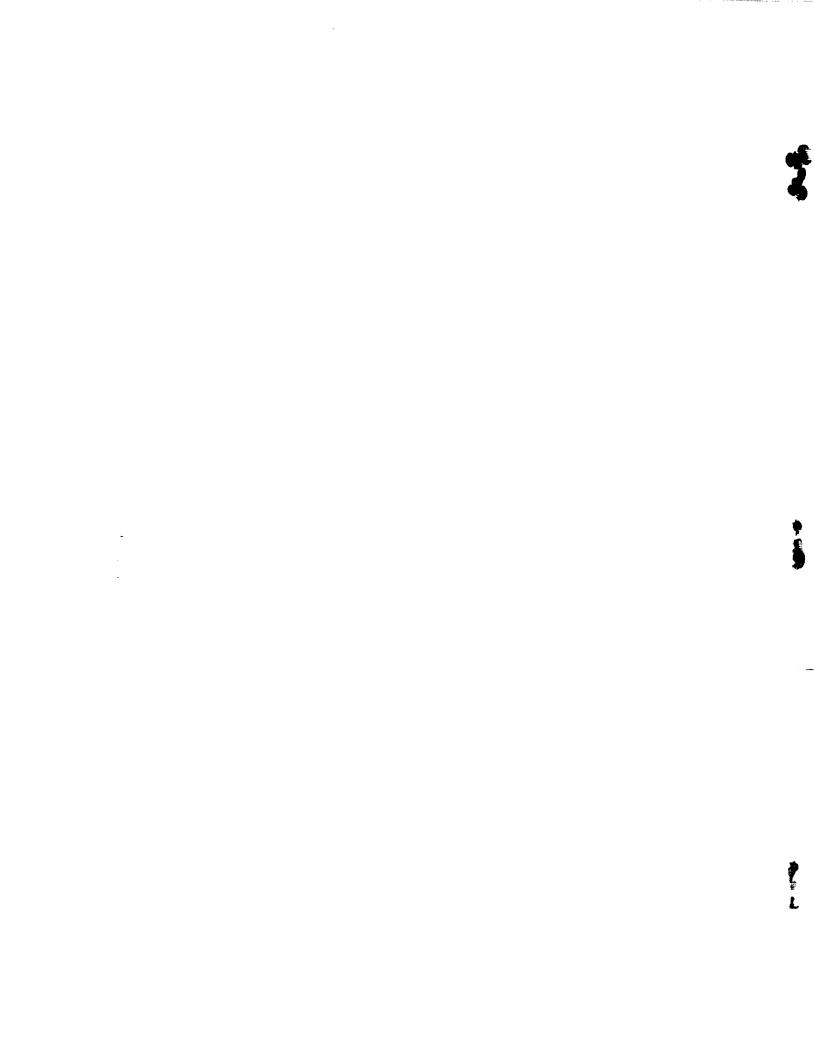
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National Aeronautics and Space Administration

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by

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## 1.0 INTRODUCTION

This report summarizes the findings of a literature study on space cured composite structures and recommends a course of future action. The information contained herein was collected from the following sources:

Chem Abstracts	1956-present
Engineering Index File	1970-present
NTIS	1964-present
COMPENDEX	1964-present
LMSC Inhouse File	1955-present
(over 178,000 catalogued books and reports)	
NASA Search	1968-present
DDC Search	1967-present

In addition a number of interviews were conducted to add further substance to the literature search. NASA/JSC, NASA/MSFC, and AFML were consulted because of past and present interests in this approach. Shell Chemical and Dow Chemical were quizzed on new matrix approaches, particularly the epoxy acrylates which combine epoxy properties with polyester type curing.

All of the literature references have been reviewed and a complete bibliography appears at the end of this discussion. The key to the report is a comprehensive table on materials and approaches for space cured composite structures. Following the table is a discussion of the most widely used approaches and materials along with comments on their viability.

Most of the applications used for demonstration of the various candidate materials and techniques involved the fabrication of solar collectors, space shelters and docking stations. In one or two cases, however, techniques were

used which could be applied to the fabrication of inflatable, space cured tubular structures. The primary matrix materials involved were gelatin, polyurethane, epoxy and unsaturated polyester. Other systems were given minimum consideration and with one exception probably will not be involved in any future work. Each of these topics is a subsection of the discussion. By far the most glaring omission is lack of data on the use of the various matrices with graphite fiber.

The approaches used to cure the various resins cited in the literature are discussed with each matrix material. The literature revealed the following curing techniques were used to rigidize the structures:

- o Plasticizer or solvent boil-off
- o Vapor reactions and/or catalysis
- o Ultraviolet radiation
- o Thermal cure
- o Elastic memory
- o Anaerobic cure

At the end of the discussion section a number of conclusions are made as to the viability of various materials and approaches. Included are suggested areas for future work. Following this are recommendations for further study prioritized in accord with the authors' feelings as to which procedures and materials have the best chance of success.

Early in the program a set of selection criteria were developed as an aid in the evaluation of the various approaches to space cured composite structures. Factors pertaining to both the fabrication and the mechanical properties of the resultant structures were considered. The criteria that were used follow:

#### Factors Pertaining to Cure and Fabrication

- 1 Tube must remain flexible during expansion
- 2 Cure should proceed at reasonable rate under ambient space conditions
- 3 Approach must provide for positive fiber alignment

# Factors Pertaining to Cure and Fabrication (cont'd)

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- 4 System must be packageable with regard to weight, volume, tack, etc.
- 5 Material must possess adequate shelf life
- 6 Process must be safe with regard to toxicity, explosion hazard, etc.
- 7 Chemistry must provide for low void content
- 8 Internal stresses resulting from shrinkage during cure should not compromise tube performance

# Factors Pertaining to Physical/Mechanical Properties

- 9 Material must be stable in space environment (vacuum, UV, radiation) for intended lifetime of the system
- 10 Matrix modulus must be in the glassy region (  $>10^9$  pa) over the temperature range of interest
- 11 Adequate strength must be maintained over the temperature range of interest
- 12 Composite should possess zero or low coefficient of thermal expansion

#### 2.0 DISCUSSION

Shown on the following page is a table which summarizes the results of this investigation. Specific matrix systems and the ways in which they rigidize and cure are listed along with the above stated selection criteria which investigators have addressed and found adequate. Possible problems associated with each matrix system are outlined and references referring to one or more of the chart headings are delineated.

#### 2.1 Gelatin Type Technology

The first category of matrix resins discussed includes those that ridigize by plasticizer or solvent boil-off. These resins do not chemically react but simply harden as they evaporate to dryness in a space environment. Gelatin has received the most attention because of several very attractive features. It is derived from abundant natural sources and should be quite economical. Flexural properties of glass laminates are good up to 250°F (121 K) and the environmental resistance to UV, IR and gamma radiation appears adequate. The main advantage to this approach is the reversible nature of the plasticizer which permits structural elements to be deployed and tested on the ground prior to packaging and flight. The primary disadvantage is the weight penalty of about 10-15% (6,43) incurred by the weight of plasticizing liquid (water) eventually lost in space. Since most of the work was done with glass fabric, compatibility with graphite is unknown. It is not known how well unidirectional fiber alignment can be maintained during rigidization or how internal stresses arising from shrinkage affect long term properties.

Much less work has been done with the other resins in this category which include polyvinyl alcohol (PVA), poly (hydroxyethyl methacrylate) [Hydron] and phenoxy. PVA requires about 23% water for plasticization and Hydron 13-14%

	wΙ	SUMMARY OF MATERIALS AND APPROACHES FOR SPACE CURED COMPOSITES	ND APPROACHES	FOR SPACE CU	ED COMPOSITES	
MATRIX SYSTEMS	RIGIDIZING PROCESS	CURE MECHANISM	SELECTION CRITERIA MET FABRICATION   PERFORMANCE	TERIA MET PERFORMANCE	POSSIBLE PROBLEMS	REFERENCES
Gelatin	Plasticizer boil-off	Physical	1,2,4,5,6,7	9,10,11	Weight penalty, high shrinkage graphite fiber compatibility	7,9,10,14,15,16, 27,28,33,35,43
PVA	Solvent boil-off	=	1,2,5,6,7	10,11	=	9
Hydron	Plasticizer boil-off	:	1,2,5,6,7	10,11	=	9
Phenoxy	Solvent boil-off	-	1,2,5	10,11	=	9
Urethane	Vapor cure	H <sub>2</sub> 0+NC0	1,2,4,6	9,10,11	Packaging, forming, blocking, fiber orientation	2,5,7,9,12,14, 15,17,18,19,23, 24,25,26,28,30, 32,34,35,39,43
Polyester	Vapor cure by tertiary amine	Accelerated peroxide, peroxide accelerated by	1,2,4,5,7	9,10,11	Blocking, cure rate, fiber orientation	2,5,9,22,23, 31,37,41,42
	UV cure	Light taccel peroxide	1,2,4,5,7	9,10,11	Cure with graphite, blocking, fiber orientation, uniform cure	4,9,13,15,22, 28,38,40,41,42, 43,44
5	IR (thermal)	Peroxide, free radicals	1,2,4,5,7	9,10,11	Blocking, fiber orientation, uniform cure	45
	Anaerobic	Loss of oxygen inhibitor	1,2,4	10	Blocking, fiber orientation	3
Epoxy	Vapor cure	Amine + resin	1,2,4,5,7	9,10,11	Blocking, fiber orientation, cure rate	11,24,31,34,
	Thermal cure	Amine + resin	1,2,4,5,6,7	9,10,11	Blocking, fiber orientation, heat source	18,22,38,40, 41
	Elastic Memory	Amine + resin	1,2,3,4,5,6	9,10,11	Heat source, resin elongation, blocking	29,36
n-Vinyl Carbazole (NVC)	Vapor cure	Volatile acid	1,2,4,5,7	10,11	Physical form of matrix, blocking, toxic, corrosive vapors	97*77
Cyclized Polybutadiene	Thermal cure	Peroxide, free radicals	2,3,4,5,6	10,11	High temperature cure	95
NVC+CPBU	Vapor cure	Heat liberated from NVC cures CPBU			Inadequate cure	46
Furfuryl Alcohol	Vapor cure	Volatile acid			Blocking, adequate cure, physical properties, corrosion, toxicity	6,37
Phenyl Silane	Vapor cure	Unknown			High pressure, high tempera- ture cure	37
Acetoxy Silane	Vapor cure	Unknown			Largely unexplored	1

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## 2.1 Gelatin Type Technology (cont'd)

and they soften at lower temperatures than gelatin., i.e.,  $185^{\circ}F$  (85 K) and  $170\text{-}200^{\circ}F$  (77-93 K), respectively. Phenoxy was dissolved in methylethylketone (MEK) which may be hazardous due to its low flash point. Phenoxy's heat distortion temperature is given as  $212^{\circ}F$  ( $100^{\circ}K$ ). A polyacrylic modified with a styrene malaic copolymer and melamine was investigated (34) but not developed to fruition.

#### 2.2 Urethanes

A great deal of work has been done with water vapor cured polyurethanes. Fiberglass laminates cured in 15-30 minutes exhibit flexural strengths comparable to those of epoxies. Large structures including cylinders 1.07m diameter and 1.2m long, a space shelter 2.1m in diameter and 2.4m high and quonset hut were fabricated from water cured a semi-cylindrical 4 by 4.6m polyurethanes. Smaller structures can be inflated from residual vapor pressure alone while larger structures require auxiliary inflation equipment. Fluted fiberglass reinforcement was used for these demonstrations. The main drawback of polyurethanes concerns shelf life. Stringent precautions must be taken to isolate the prepreg from moisture to prevent premature hardening. This necessitates impermeable packaging which introduces a weight penalty and a disposal problem. Available literature indicates only slight degradation of flexural modulus for two urethane resins when exposed to IR and UV radiation over the course of 4 weeks. The effects of longer exposure are unknown. The chemistry of polyurethanes cured in this manner evolve carbon dioxide which can cause foaming, depending on the rate of reaction. pears, however, that this concern is not as serious as anticipated.

#### 2.3 Polyesters

Polyesters cured by vapor catalysis, UV radiation or IR (heat) have been investigated for rigidizable space structures. Mechanical properties are adequate but degradation due to continuous exposure to UV and gamma radiation is suggested by the limited data on hand (2). UV cures are very fast and deployment times may not be sufficient enough to assure dimensional stability

## 2.3 Polyesters (cont'd)

prior to rigidization. It should be noted that in a discussion with Hexcel they stated they were unable to obtain UV cures in graphite composites.

Shrinkage is rather high with polyesters in general and high internal stresses could develop if adequate measures are not taken to insure uniform exposure during cure. High shrinkage combined with poor adhesion in general point to loss of strength with aging. IR cure also requires uniform exposure to the sun and resins conducive to this type of cure remain warm during service, thereby functioning with reduced strength (43). Gas catalysis appears to be the most viable approach for polyesters. However, this approach requires special packaging containers and the associated weight penalty.

## 2.4 Epoxy Resin Technology

Three rigidizing methods for cured in space epoxy matrix composite structures have been studied; vapor cure, thermal cure and elastic memory. Of the three methods, vapor curing has apparently received the most attention. Numerous catalysts and curing agents have been tried including Lewis bases such as tertiary amines and triphenylphosphine and Lewis acids such as stannic chloride and diamines such as 1,3-propylene diamine and 1,4-cyclohexane bis (methyl amine). Surprisingly, the use of ammonia as a curing agent could not be found in the literature. In our interviews, Dr. R. W. Tess of Shell Chemical stated that he was able to cure surface coatings up to 10 mils in thickness using this technique. It was claimed that poly (allyl glycidyl ether) gave excellent coatings.

Another technique that received considerable attention was that of heat curing systems. This approach has the advantage of being able to choose from a wide variety of curing agents but this can cause shelf life problems. Probably the best system for this purpose would be a "kicked dicy" formulation. These systems have almost infinite pot life and cure around 246°F (119 K). We have calculated that using resistance heating (wires in the composite) the power required to cure a 15.2cm diameter tube 0.76mm thick and 9.1m long at 250°F (121 K) in space, in the absence of sunlight, would require a solar cell power

## 2.4 Epoxy Resin Technology (cont'd)

panel area of 46 square meters. Perhaps a weight penalty could be avoided by using the graphite fibers as the resistance element.

Another technique which was mentioned briefly in the literature is that of elastic memory. One of the authors holds patent rights on this concept involving epoxy resins. Elastic memory is the ability of a deformed thermoset structure to regain its original shape.

At its glass transition temperature (Tg) a thermoset matrix has a low modulus and displays high elongation to break. Under these conditions it can be pressed into another shape and if held in this condition during cooling it retains the strained, collapsed shape indefinitely. However, when reheated above its Tg the structure regains its original shape without external force. Thus a tubular structure could be collapsed and reformed in space simply by heating. One article was found in the literature indicating the feasibility of the approach. The concept was demonstrated using glass fibers embedded in an epoxy matrix to form a collapsible aircraft wing tank for packaging during transport. The idea has not been considered for space applications. This could be a high payoff area.

Our visits to Shell and Dow revealed an interesting new raw material in the epoxy acrylates (trade names EPOCRYL and DERAKANE). These materials are available in a variety of forms and cure like a polyester but have epoxy type properties. Accordingly, the rigidizing technology used would be identical with that discussed in the previous section under Polyesters.

From the standpoint of structural integrity and proven characteristics with graphite fibers the epoxies as a class are ideal candidates. In addition to that of selecting the curing agents the major problem appears to be one of blocking (the tendency of adjacent layers of prepreg to stick to each other) which complicates high density packaging concepts. It is, of course, possible to use barrier films to prevent blocking but this complicates the manufacturing process. There are other possible solutions to this problem. One is to

# 2.4 Epoxy Resin Technology (cont'd)

partially react the product to a non-tacky, rubbery gelled state and use a second curing agent to complete the process. Another is to incorporate an elastomer in the formulation in sufficient quantity to eliminate the tack and harden the tube with a second curative. A third approach would be to chemically react the outer surface of the composite layup. For example, the epoxy acrylates contain a plurality of hydroxyl groups on the backbone structure which might be used in conjunction with a diisocyanate to form the surface skin.

## 2.5 Miscellaneous Resin Systems

The most promising matrix system which falls under none of the above categories is a cyclized polybutadiene urethane (CPBU) developed by TRW under an LMSC subcontract(46). The resin displays good compressive and flexure strengths up to 500°F (260 K) after thermal cure at 350°F (177 K). While this particular resin requires extensive thermal energy (4 kw-min/sq ft for prepreg on fluted glass fabric) in order to reach 350°F (177 K), the method offers the following distinct advantage. The matrix resin is prepregged and then B-staged (partially cured) to a flexible non-tacky, rubbery state which provides excellent packaging characteristics - no shelf life problem and no weighty impermeable containers. In addition, the fiber alignment is maintained by the rubbery state. By following a similar B-staging approach with a 250°F (121 K) or lower curing resin on graphite one might circumvent the current deficiency, especially if the graphite fibers could be used for resistance heating.

N-vinyl carbazole showed some promise as a 93-121 K matrix system although the gas required for catalysis, viz. dinitrogen tetroxide, is highly corrosive and toxic. There is an added complication in that N-vinyl carbazole is a crystalline solid. A combination of N-vinyl carbozole and CPBU was found to be unworkable.

Furfural alcohol cured with HCl gas shows no promise due to slow cures and poor strengths coupled with the highly toxic and corrosive nature of the

## 2.5 Miscellaneous Resin Systems (cont'd)

catalyst. A vapor cure for a modified phenyl silane was briefly investigated until it was realized that high temperatures and pressures were required for suitable fabrication. An acetoxy silane was under development when Air Force funding limitations apparently cut this effort short.

#### 3.0 CONCLUSIONS

The most widely studied matrix resin appears to be gelatin. It exhibits good mechanical properties to 121K and space environmental exposure data (UV,IR,gamma radiation) looks good. A strong selling feature is the reversibility which permits terestial quality control. The main deficiencies are the weight penalty of plasticizer (water) and substantial shrinkage stresses which may prove troublesome upon aging. No data are available with graphite fibers. Any future work should address the potential shrinkage problem and generate data on graphite fibers.

Water cured polyurethanes have received considerable attention and large scale demonstrations have been successful. Properties are quite satisfactory. Perhaps the biggest drawback is the stringent requirement that water vapor be excluded during storage. Therefore a barrier weight penalty is exacted in addition to the weight of water required for cure.

Polyesters have received less attention than either of the above systems. UV cured polyesters require a uniform exposure during cure and will not necessarily work with graphite fibers. However, amine vapors can be used to initiate cure of peroxide catalyzed systems. With the advent of newer systems such as the epoxy acrylates, superior properties could be realized. This area warrants further investigation.

Epoxy resins have not really received adequate evaluation in light of their proven properties as matrix resins for graphite reinforced composites. A recent visit to Shell Development Company in Houston, Texas, has directed our attention to considerable success which they have had with ammonia vapor cures of epoxy systems. Utilization of this approach was not found in our cured-in-space literature search.

## 3.0 Conclusions (cont'd)

A cyclized polybutadiene urethane, while not desirable as a material per se, was interesting from a processing standpoint. B-staging a resin to a non-tacky, rubbery state offers a weight savings in terms of eliminating separator films and provides for positive fiber alignment during deployment and cure.

The "elastic memory" approach demonstrated for an epoxy formulation but applicable to other materials as well holds considerable potential. The technique can be reversible, provide for positive fiber alignment and provide desirable packaging characteristics while offering satisfactory physical/mechanical properties. Although this approach may be considered high-risk/high payoff, these features provide high reliability and ease of handle-ability unattainable by other approaches. Since a well controlled heating rate is not as critical for the elastic memory approach as for one involving chemical cure a solar concentrator may offer adequate energy for deployment.

## 4.0 RECOMMENDATIONS FOR FUTURE EFFORT

Listed below are a series of general concepts which should be considered for future work. They have been prioritized based on the author's analysis of the data available, the topmost idea being considered as the best.

- o The elastic memory concept should be studied further. Although this is a high risk approach the rewards appear great. An epoxy/graphite system is the recommended starting point.
- o Develop the concept of non-tacky pliable composite layup in order to minimize packaging. Using epoxies and/or epoxy acrylates through chemical reaction, partial gelatin or elastomer inclusion make a non-blocking packageable system which can be subsequently cured to a rigid structure.
- o Generate further data on the evaporative rigidization concept answering such questions as the effect of graphite fibers and the plausibility of other matrices of this type.

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## REFERENCES 1

- 1. Ault, G. R., <u>Self Rigidizing Expandable Sandwich Aerospace Shelters and Solar Collectors</u>, Archer Daniels Midland Co. and Goodyear Aerospace Corp., Contract AF33(615)2435, Progress Report for Period Ending May 15, 1965
- 2. Ault, G. R., <u>Self Rigidizing Expandable Sandwich Aerospace Shelters and Solar Collectors</u>, Archer Daniels Midland Co. and Goodyear Aerospace Corp., Contract AF33(615)2435, Progress Report for Period Ending May 15, 1966
- 3. Barnes, R. F., "Anaerobic Adhesives for Structural Aircraft Bonding" SAMPE National Technical Conference, Vol 1, Sept 1969
- 4. Cheorvas, W., Chemical Rigidization Space Structures, Independent Development Report No. 18514, Lockheed California Co. June 28, 1965
- 5. Clemens, L. M, McKillip, W. J, and Lee, J., "Vapor Cured Resins for Aerospace Applications", National SAMPE Symposium, Vol. 11, 1967
- 6. Cordier, K. L., Optimization of Chemically Rigidized Expandable Structures
  Technology, Goodyear Aerospace Corp., AF Contract F33615-69-C-1224,
  AFAPL-TR-70-19, May 1970
- 7. Crawford, J. E. and Blackwell, E. G., <u>Project AHT</u>, Space General Corp., Contract AF33(615)3469, AFAPL-TR-67-30, April 1967
- 8. Evans, G. R., Expandable Structures in Space: An Annotated Bibliography, Lockheed Missiles and Space Co., Special Bibliography SB-63-36, Navy Contract NOW 62-0363, April 1963
- 9. Forbes, F.W., Expandable Structures for Space Applications, AF Aero Propulsion Laboratory, DDC Report AD 607 541, July 1964
- 10. Forbes, F. W. et al, "Gelatin, A Rigidizing Material for Aerospace Structures", pp 192-215 in Aerospace Expandable Structures Conference Transactions sponsored by AFAPL and AFFDL Dayton, Ohio, Oct 1963
- 11. Graham, T.L., <u>Expandable Rigidizable Structures</u>, Air Force Materials Laboratory, ASD-TDR-62-311, May 1962
- 12. Graham, T. L., and Spain, R. G., "Rigidization of Expandable Structures via Gas Catalysis" pp 236-254 in <u>Aerospace Expandable Structures</u>

  <u>Conference Transactions</u> sponsored by AFAPL and AFFDL, Dayton, Ohio,
  Oct 1963

Alphabetical listing by author(s)

#### REFERENCES (cont'd)

- 13. Hanny, J. F, Lankston, L. R, Jones, J. W. and Scott, J. C., <u>Chemical Rigidization of Expandable Structures</u>, the National Cash Register Co., Contract AF-33(615)-2684, AFAPL-TR-66-53, Sept 1966
- 14. Jurich, L. and Hose, R. L., <u>Applications Study of Expandable Space Structures</u>, Goodyear Aerospace Corp., AF Contract F33615-69-C-1125, AFAPL-TR-70-45, Nov 1970
- 15. Keller, L. B. and Schwartz, S., <u>Rigidization Techniques for Integrally Woven Composite Constructions</u>, Hughes Aircraft Corp., Contract AF33(657)-11287, ML-TDR-64-299, Sept 1964
- 16. Keller, L. B. and Schwartz, S., <u>Rigidization Techniques for Integrally Woven Composite Constructions</u>, Hughes Aircraft Corp., Contract AF33(657)-11287, AFML-TR-65-402, Dec 1965
- 17. Knox, P. M., Expandable Space Structure Semirigid or Nonrigid Structures for Space Application, Martin-Marietta Corp., Contract AF33(657)-9733, ML-TDR-64-281, Vol I "Report Summary", Sept 1964
- 18. Knox, P. M., Expandable Space Structure Semirigid or Nonrigid Structures for Space Application, Martin-Marietta Corp., Contract AF33(657)-9733
  ML-TDR-64-281, Vol II "Appendices", Sept 1964
- 19. Latture, N. C., <u>Vacuum Testing of Expandable Self-Rigidizing Structures</u>, Arnold Engineering Development Center, AEDC-TR-65-264, Dec 1965
- 20. Liddell, R. B., <u>Study of Expandable Structures</u>, Lockheed California Co., Contract AF33(657)-8776, AD 295068, Progress Report, Oct 1962
- 21. Liddell, R. B., Expandable Structures Design Handbook, Lockheed California Co., Contract AF33(657)-8776, RTD-TDR-63-4275, Part I, June 1965
- 22. Liddell, R. B., Expandable Structures Design Handbook, Lockheed California Co., Contract AF33(657)-8776, RTD-TDR-63-4275, Part II, June 1965
- 23. McKillip, W. J., Nordstrom, J. D., and Dunning, E. B., "The Development and Optimization of a Resin System for Rigidization of Expandable Honeycomb Structures", Report presented at the 20th Annual Meeting of the Reinforced Plastics Division, SPI, held in Chicago, Ill., 1965
- 24. McKillip, W. J., Clemens, L. M., Leitheiser, R. H., Lee, J., and Impola, C. N., "Development and Optimization of Resin Systems for Expandable Honeycombs",pp 19-49 in Second Aerospace Expandable Structures Conference Transactions, AFAPL-TR-65-108, May 1965

## REFERENCES (cont'd)

- 25. McKillip, W. J., Lee, J., and French, R., "Gas-Cured Urethane Resin Systems for Space Structures", pp 89-103 in <u>Third Aerospace Expandable</u> and Modular Structures Conference Transactions, AFAPL-TR-68-17, May 1967
- 26. McKillip, W. J., French, R. J., et al <u>Vapor Rigidized Expandable Solar Collector and Aerospace Cylinders</u>, Archer Daniels Midland Co. and Goodyear Aerospace Corp., Contract AF33(615)-2435, AFAPL-TR-66-149, May 1967
- 27. Neaman, R. G., <u>Gelatin Rigidized Expandable Sandwich Solar Energy Concentrators and Space Shelters</u>, G. T. Schjeldahl Co., Contract AF33(615)-2058, AFAPL-TR-66-135, Aug 1966
- 28. Olevitch, A., Allinokov, S. A., Keller, L. B., and Schwartz, S. S., "Space Rigidized Resin Fiberglass Sandwich Materials", <u>J. Spacecraft</u>, Vol 3, pp 513-518, Apr 1966
- 29. Pezdirtz, G. F., "Erectable Space Structures Echo Satellites"
  National SAMPE Symposium, May 1962
- 30. Quigley, R. E., <u>Deployment and Rigidization Test of a Large Inflatable Solar Collector</u>, AFAPL Inhouse, AFAPL-TR-67-37, Apr 1967
- 31. Rochon, R., Clark, R. C., Hanssen, N. S., and McKillip, W. J., Aerospace Expandable Structures and Maintenance Support Devices, GCA Corp and Archer Daniels Midland Co., Contract AF33(615)-1243, AFAPL-TR-65-40, Vol. 1, July 1965
- 32. Rochon, R., and Neaman, R. G., <u>The Design, Fabrication, Expansion, and Rigidization of Model and Full Size Space Type Cylinder Structures</u>, G. T. Schjeldahl Co., Contract AF33(615)-2115, AFAPL-TR-66-100, Oct 1966
- 33. Russell, I. W., and Hanssen, N. S., <u>The Application of a Gelatin Resin System to Aerospace Expandable Sandwich Structures</u>, GCA Corp., Contract AF33(615)-2058, AFAPL-TR-65-84, Oct 1965
- 34. Russell, I, Hannssen, N., McKillip, W., and Culbertson, B., "Expandable Self-Rigidizing Honeycomb Structures", pp 168-191 in Aerospace Expandable Structures Conference Transactions sponsored by AFAPL and AFFDL, Dayton, Ohio, Oct 1963
- 35. Russell, I. W., "The Application of Expandable Honeycomb to the Fabrication of Space Structures", pp 51-73 in Second Aerospace Expandable Structures Conference Transactions, AFAPL-TR-65-108, May 1965

#### REFERENCES (cont'd)

- 36. Saylor, I. O., Zappanti, A., Olevitch, A., Ross, R. S., et al "Expandable Wing Tanks for Aircraft", pp 589-629 in Third Aerospace Expandable and Modular Structures Conference Transactions, AFAPL-TR-68-17, May 1967
- 37. Schaumberg, W. H., and Dunning, E. B., <u>Development of an Inflatable Self-Rigidizing Space Shelter and Solar Collector from Honeycomb Sandwich Material</u>, GCA Corp and Archer Daniels Midland Co., Contract AF33(657)-10409, AFAPL-TDR-64-29, Apr 1964
- 38. Schwartz, S. and Zelman, I. M., "Automatic Rigidization for Inflatable Satellites", Space Aeronautics, pp 69-71, June 1962
- 39. Schwartz, S., <u>Delayed Action Foam-in-Place Polyurethane for Use in an Aerospace Environment</u>, Hughes Aircraft Corp., Contract AF 33616-7925, ASD-TDR-62-416, March 1963
- 40. Schwartz, S., Jones, R. W., and Keller, L. B., "Ultraviolet and Heat Rigidization of Inflatable Space Structures", pp 369-380 in Aerospace Expandable Structures Conference Transactions sponsored by AFAPL and AFFDL, Dayton, Ohio, Oct 1963
- 41. Schwartz, S., "Development of Space Expanded and Rigidized Solar Energy Collectors", pp 555-571 in Second Aerospace Expandable Structures Conference Transactions, AFAPL-TR-65-108, May 1965
- 42. Schwartz, S. and Bagby, J., <u>Rigidized Inflatable Solar Energy Concentrators</u>, Hughes Aircraft Corp., Contract NAS1-3244, NASA CR-254, July 1965
- 43. Schwartz, S. and Keller, L. B., "Automatic Curing of Reinforced Plastics in Space", pp 707-736 in <u>Third Aerospace Expandable and Modular Structures Conference Transactions</u>, AFAPL-TR-68-17, May 1967
- 44. Schwartz, S., "Space Rigidization Techniques for Expandable Structures", 15th National SAMPE Symposium, pp 1073-1088, 1969
- 45. Taffe, J. B., <u>Definitive Experiment Plan SIVB/DO-22 Experiment Structures</u>
  <u>for Recovery</u>, Lockheed Missiles and Space Co., Contract F33615-67-C-1403,
  Report LMSC/A837974E, June 1968
- 46. Taffe, J. B., Encap Vehicle, Lockheed Missiles and Space Co., Contract F33615-68-C-1259, AFAPL-TR-68-117, Vol I 'Optimization and Evaluation of Four Resin Systems', Oct 1968
- 47. Yarymovych, M. I., and Forbes, F. W., "Expandable and Modular Structures Technology for Support of Manned Missions", presented at XVII International Astronautical Federation Congress, Madrid Spain, AFAPL-Conf-67-5, Oct 1966